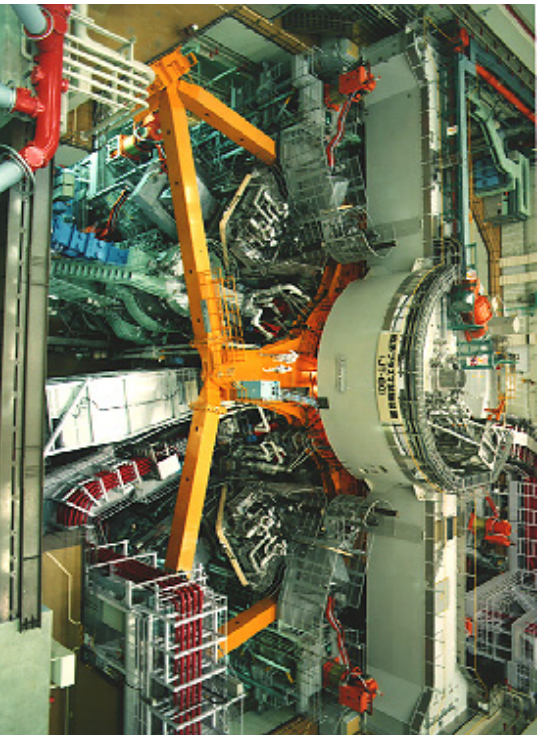


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Compatibility of Advanced Tokamak Plasma with High Density and High Radiation Loss Operation in JT-60U

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Introduction

JT-60U

Advanced tokamak plasma with **internal transport barrier (ITB)**

- Reversed shear (**RS**) plasma
- High β_p H-mode plasma (weak positive shear)

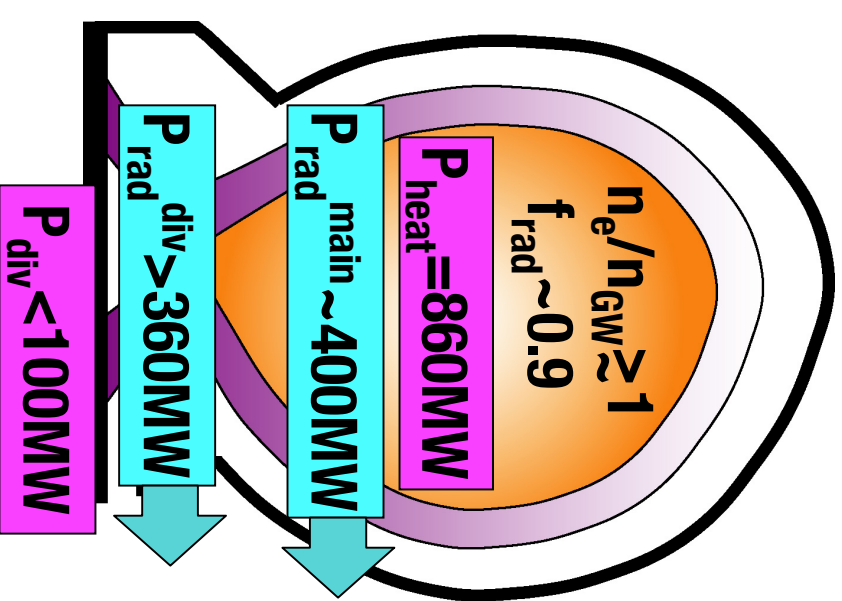
Density ITB

- Advantage for high density operation **above the Greenwald density (n_{GW})**
- Concern for high-Z impurity accumulation
 - Radiative cooling in the core plasma
 - Fuel dilution

↔ Compatible ?

High density & high radiation loss operation

- Demonstration of high density operation above n_{GW}
- What happens with strong impurity accumulation ?



Example for A-SSTR2

Contents

JT-60U

1. Extension of operation regime

- High density with high confinement and high radiation loss fraction

2. Reversed shear plasma

- High density operation
- Impurity accumulation
- Enhancement of divertor radiation by impurity seeding

3. High β_p H-mode plasma

- High density operation with HFS pellets and impurity seeding
- Mechanism of confinement improvement
- Impurity transport

4. Discussion of applicability of impurity seeding to fusion reactor

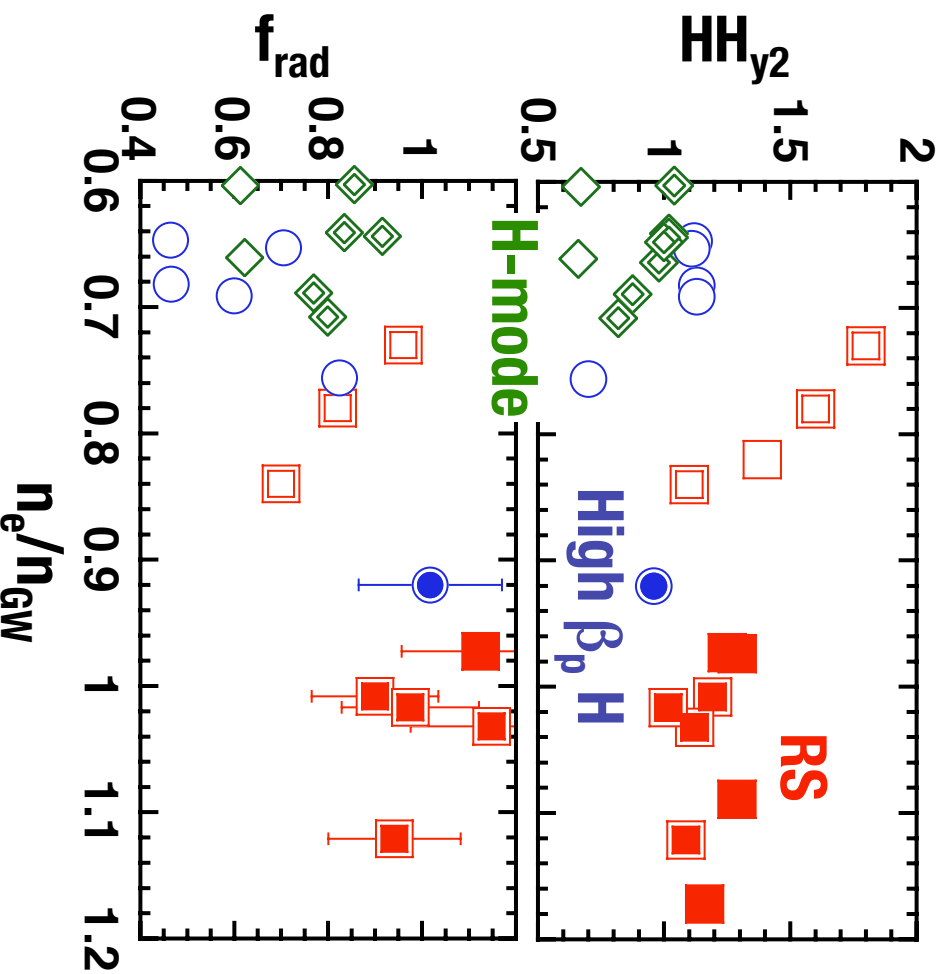
- Dependence on density peaking and impurity accumulation

5. Summary

1. Extended regime to high density

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- **Operation regime has been extended to high density ($n_e/n_{GW} \gtrsim 1$) with high confinement ($HH_{y2} \gtrsim 1$) and high radiation loss fraction ($f_{rad} > 0.9$).**



Key : ITB control

- Fueling (NB, HFS pellet and gas-puffing)
- Heating
- Impurity seeding
- (Intrinsic impurity)
- Plasma configuration

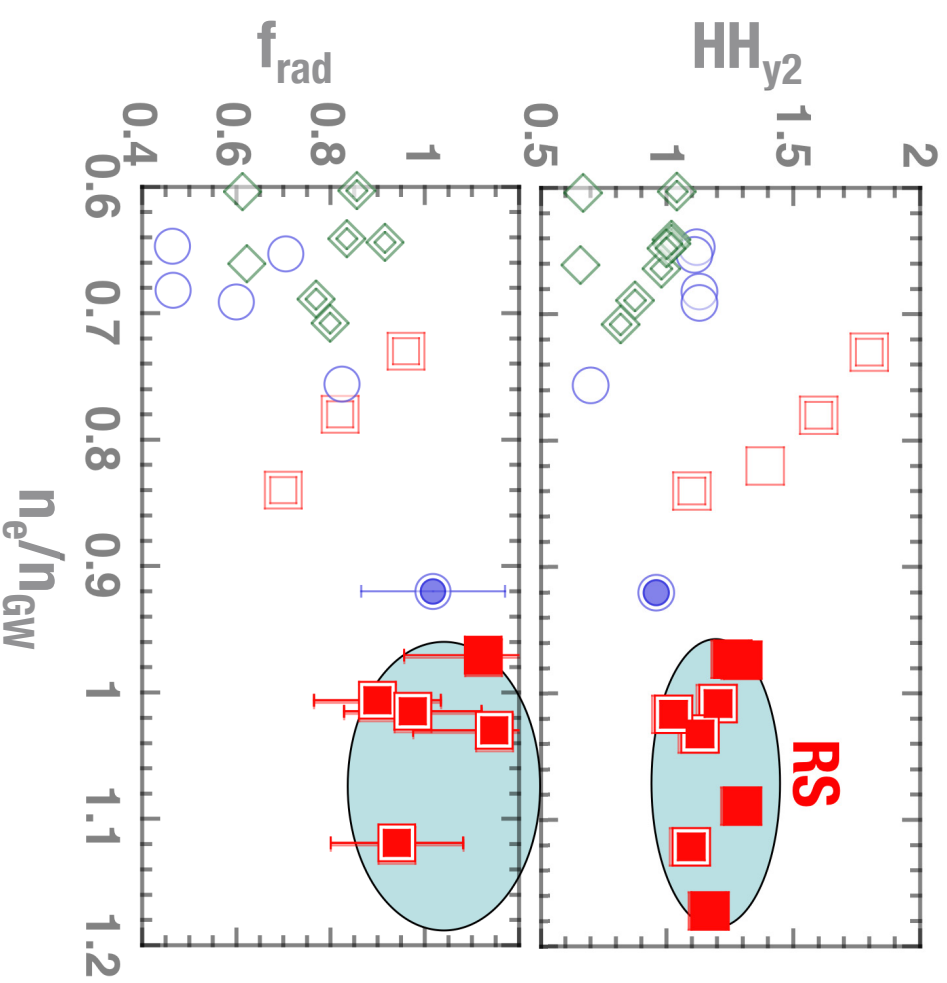
Closed : New, Open : Old

Double lines : w impurity seeding

2. Reversed shear plasma

JT-60U

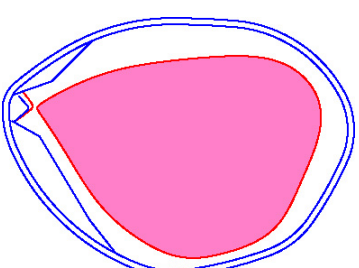
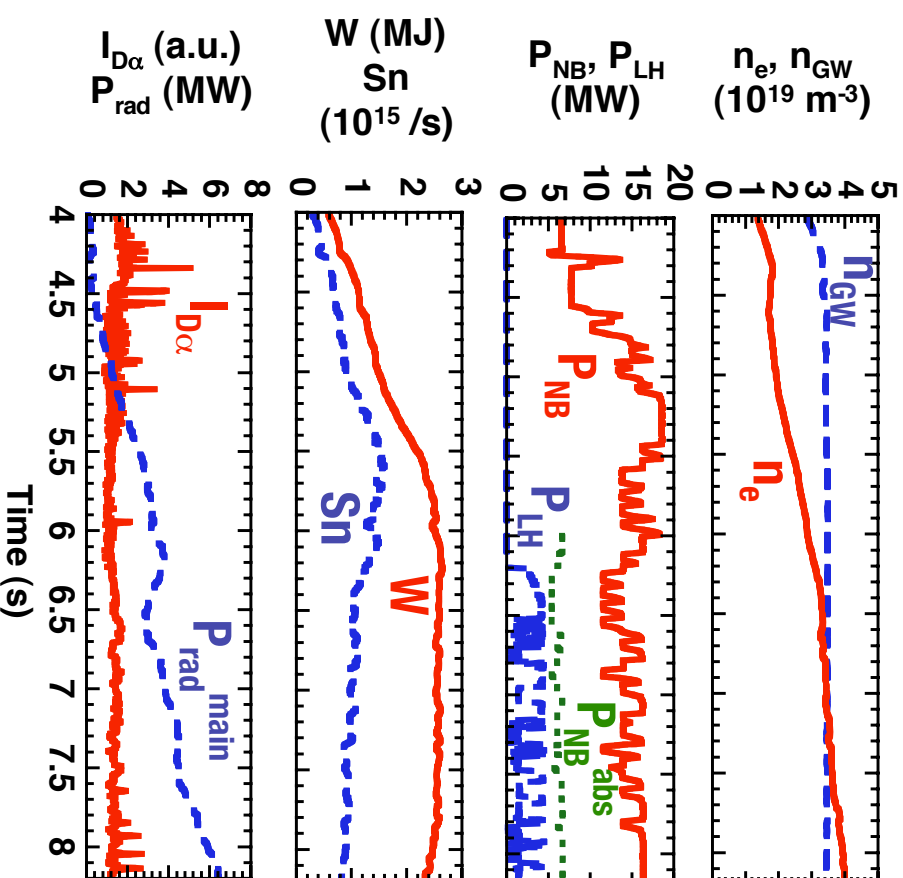
- High density operation
- Impurity accumulation
- Enhancement of divertor radiation by impurity seeding



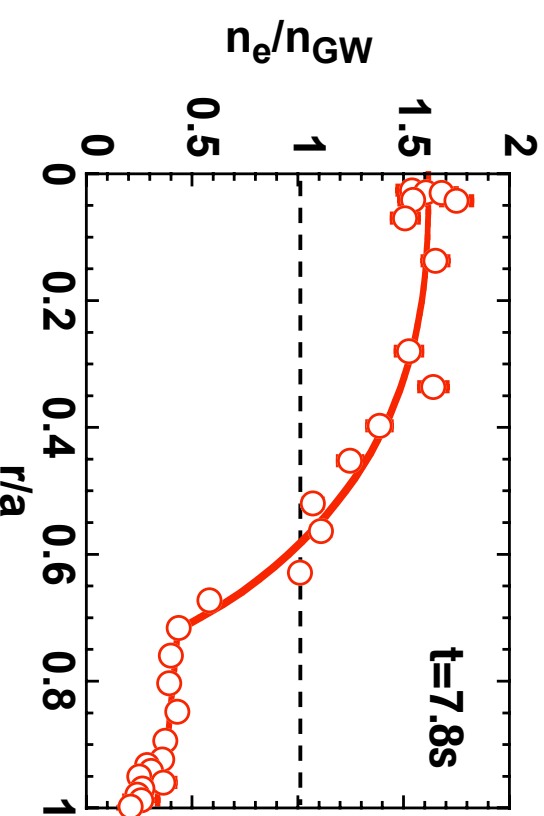
High n_e above n_{GW} in RS plasma

JT-60U

- Large V_p with NB and LH heating, and NB fueling only.
- $HH_{y^2}=1.3$, $\beta_N=2$ and $f_{BS}\sim 0.7$ at $n_e/n_{GW}=1.1$.
- $n_e(0)/n_{GW}=1.6$ with low $n_{e\ edge}/n_{GW}$ (~ 0.4) by tailoring n_e ITB.
- Increase in $P_{rad\ main}$ ($P_{rad\ main}/P_{abs}\sim 0.65$) due to impurity accumulation.



$I_p=1.0$ MA, $B_T=2.5$ T,
 $q_{gs}=6.1$, $\delta=0.45$,
 $V_p=78$ m³

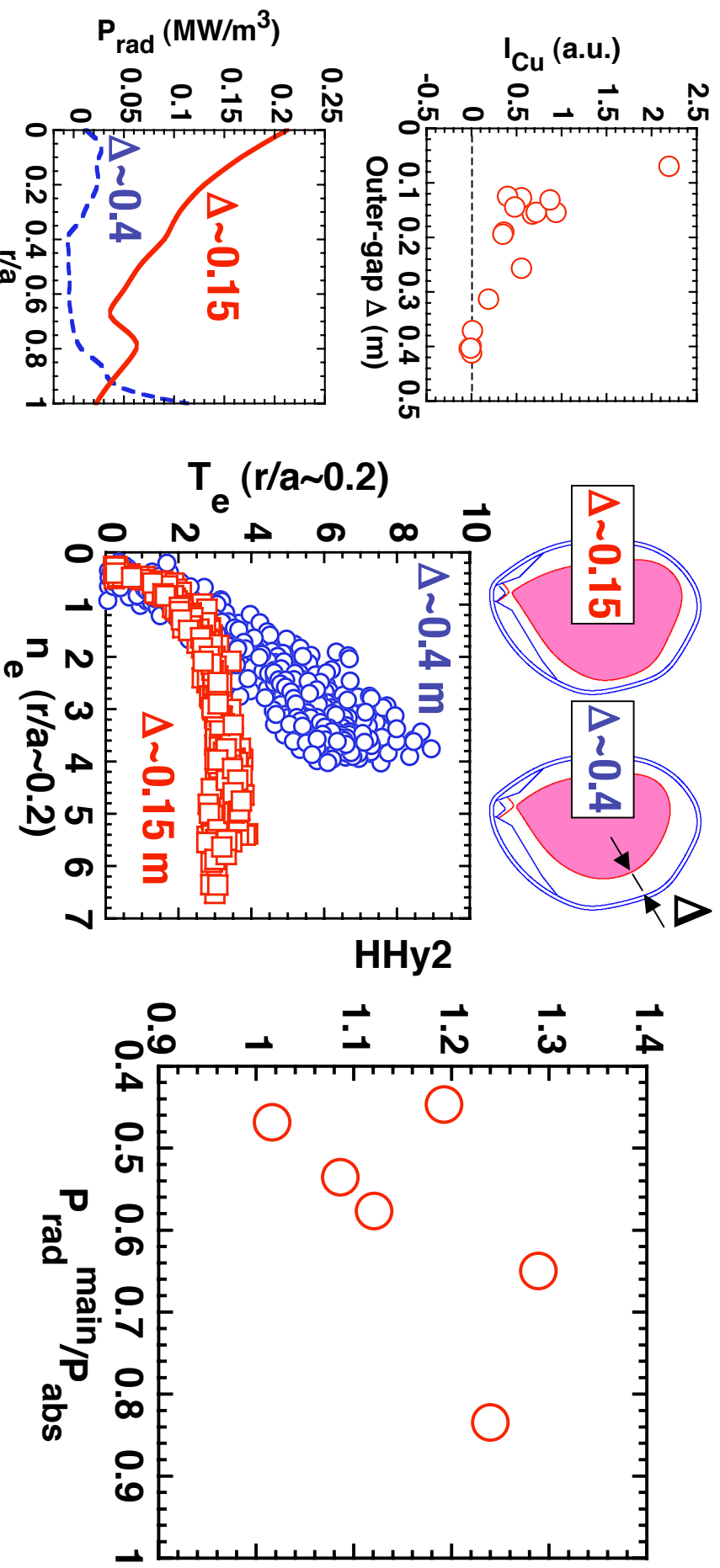


Increase in n_e with constant T_e inside ITB at small outer-gap

JT-60U

- Cu line intensity increases with decreasing the outer-gap (Δ).
- Off-axis heating, radiative cooling and NB fueling could be responsible for relationship between central n_e and T_e .

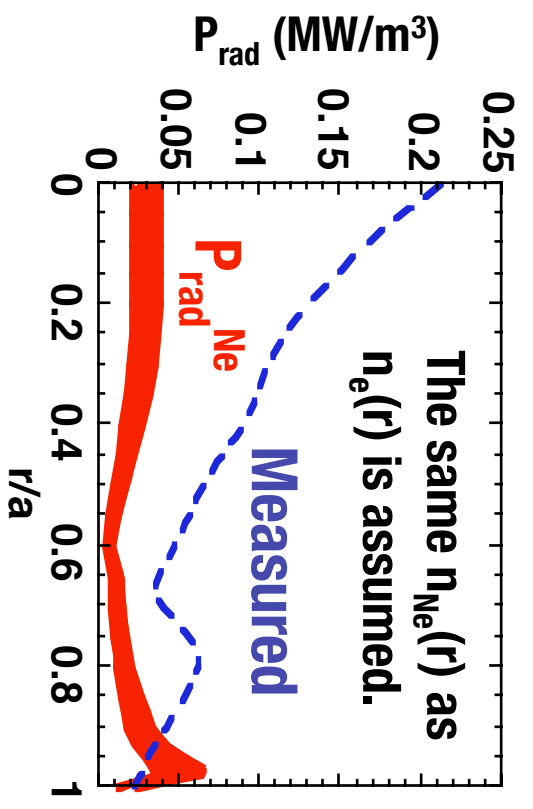
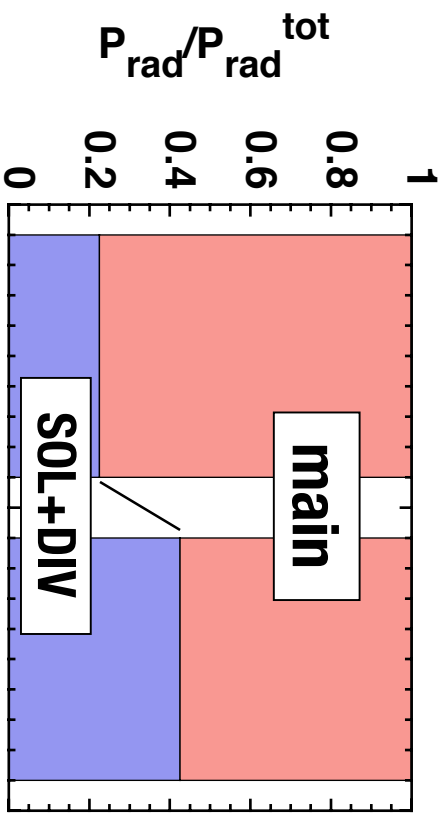
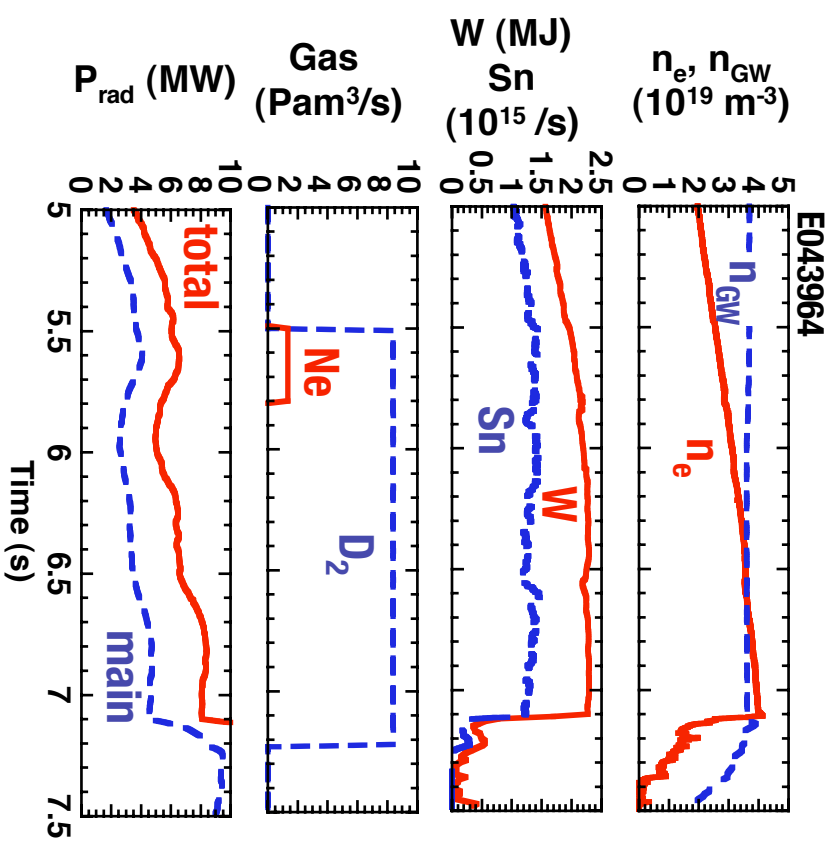
- **$HH_{y2} = 1.2$ with $P_{\text{rad main}}/P_{\text{abs}} \sim 0.8$.**



Enhanced divertor radiation by Ne seeding

JT-60U

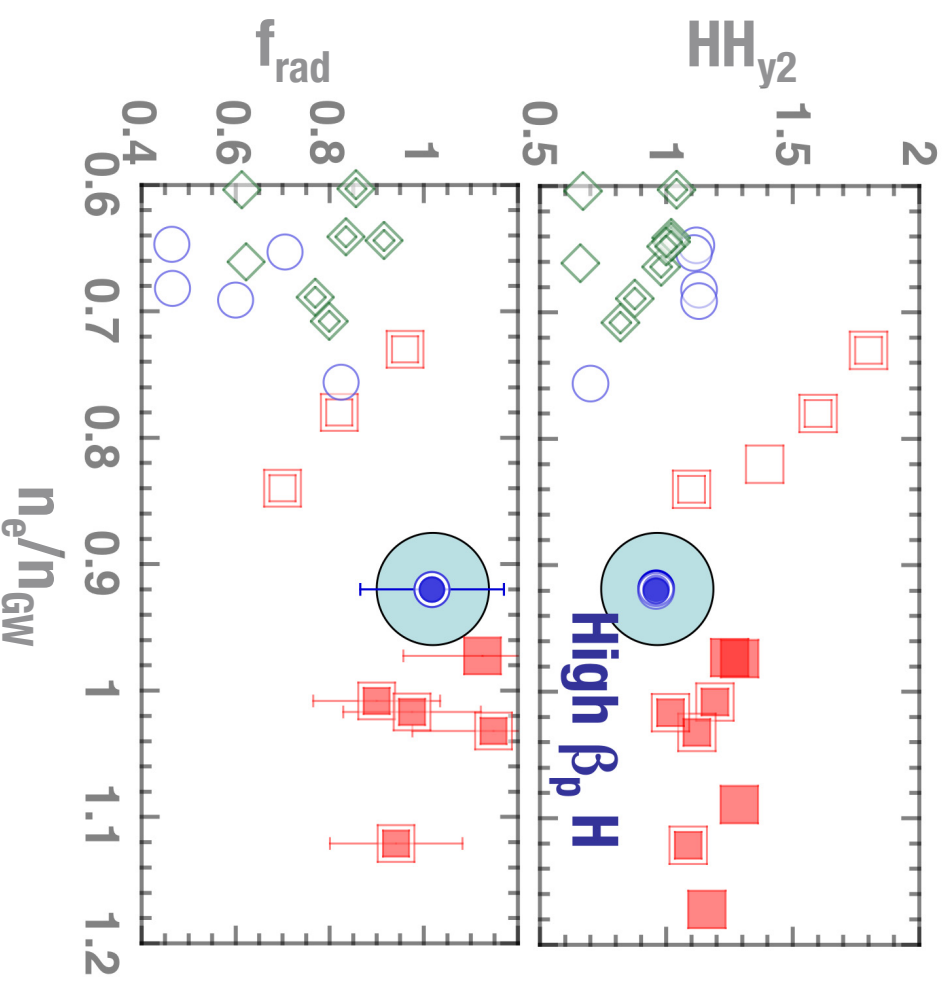
- Ne puff with D₂ gas at Δ=0.13 m.
- **HH_{y2}=1.1, f_{rad}=0.93** at n_e/n_{GW}=1.1.
- Divertor radiation ratio increases from ~20% w/o seeding to 40% with Ne seeding.
- Small contribution of Ne to P_{rad main}.



3. High β_p H-mode plasma

JT-60U

- High density operation with HFS pellets and impurity seeding
- Mechanism of confinement improvement
- Impurity transport



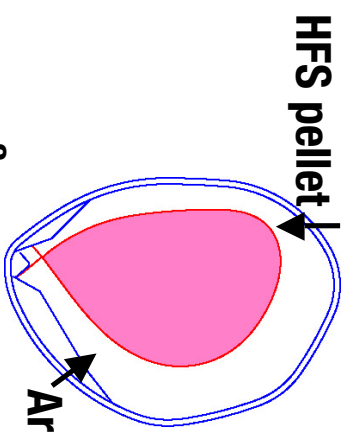
High HH_{y2} and high f_{rad} by Ar seeding and HFS pellets

JT-60U

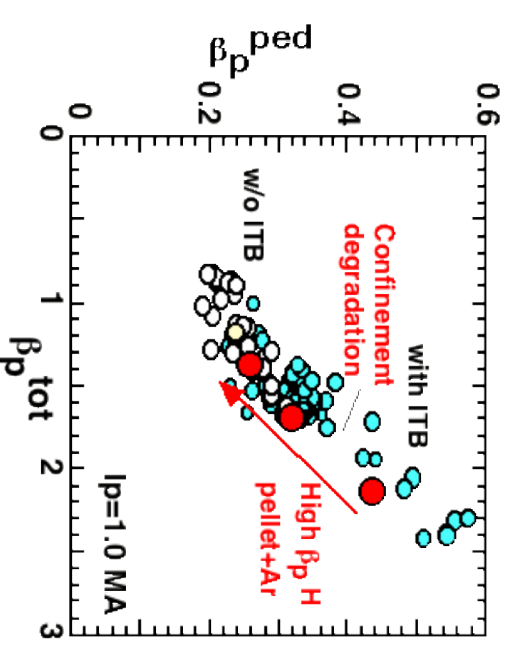
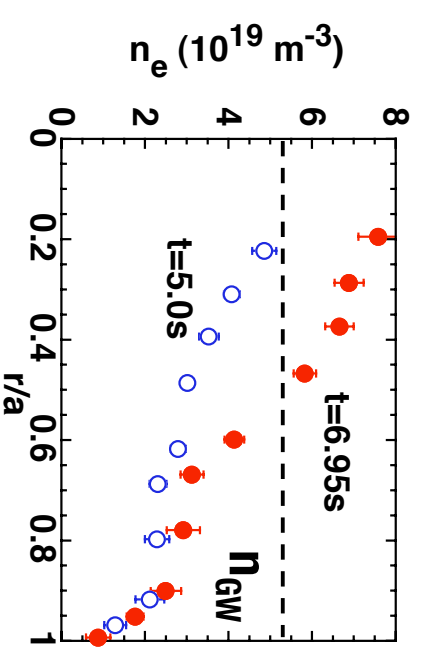
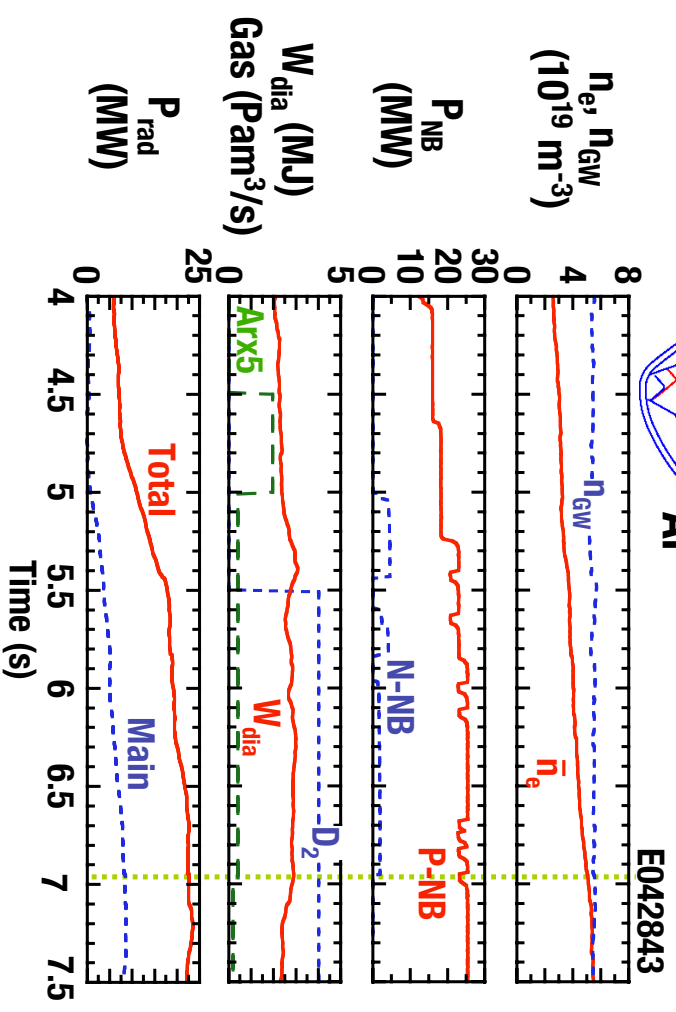
- Ar seeding and HFS pellet with small D_2 gas-puffing in small V_p .

• $HH_{y2}=0.96$ and $f_{rad}\sim 1$ at $n_e/n_{GW}\sim 0.92$ at $t=6.95s$.

• Peaking of $n_e(r)$ and enhanced pedestal pressure.



$I_p=1.0MA, B_T=3.6T,$
 $q_{95}=6.2, \delta=0.37$



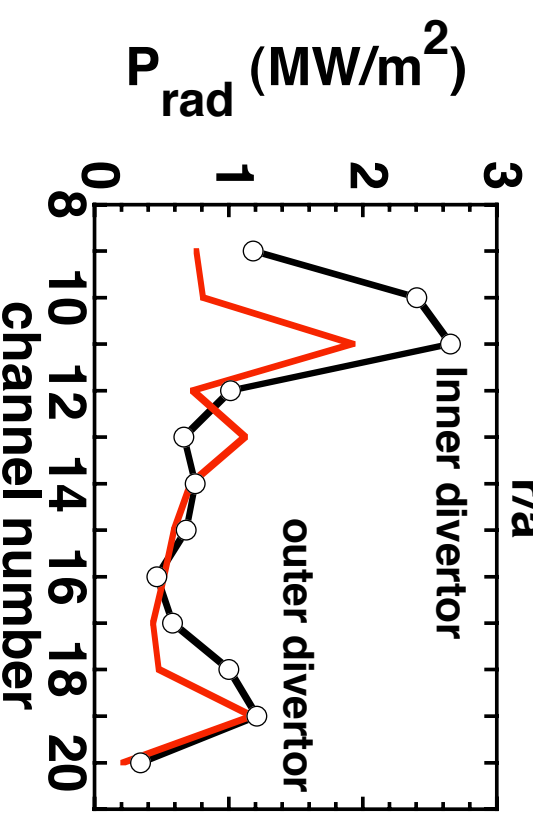
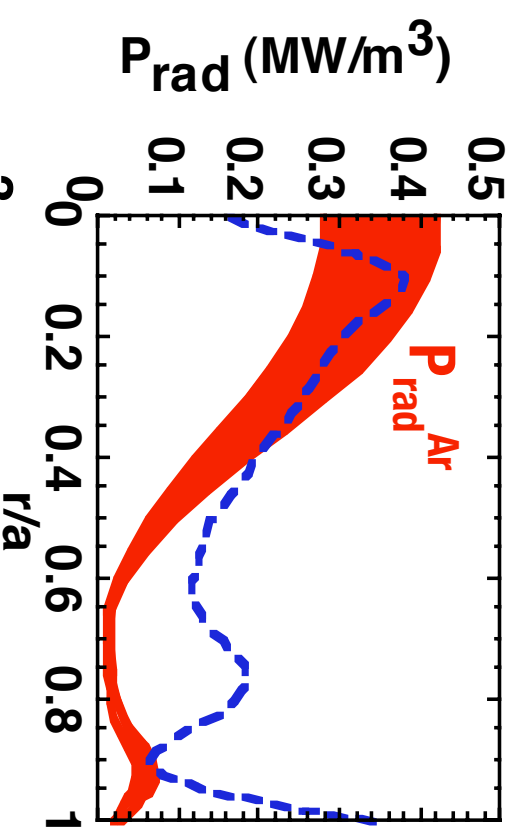
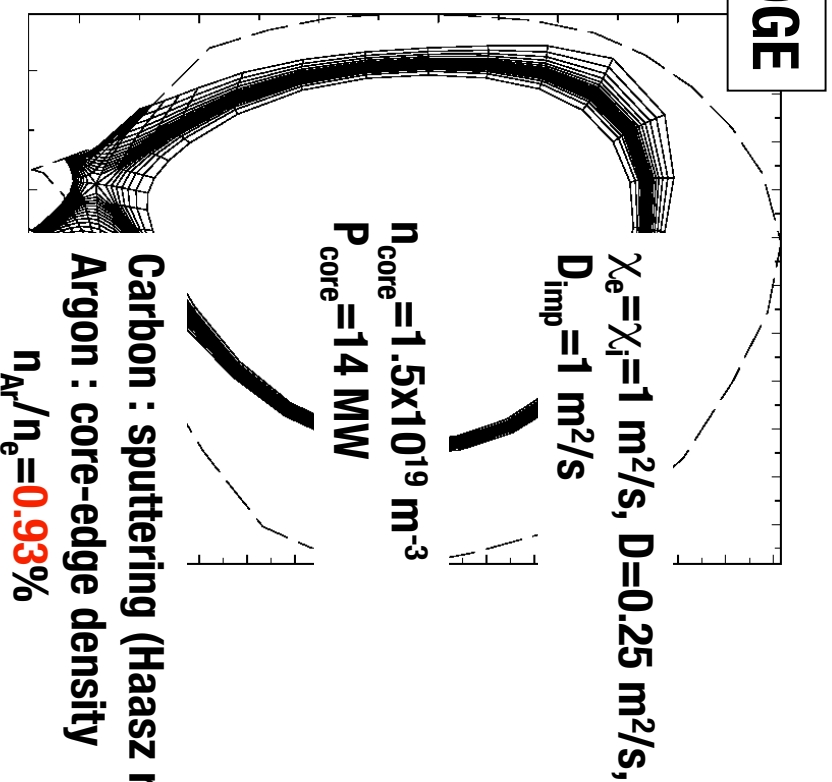
Central radiation is ascribed to Ar

JT-60U

- $n_{Ar}(r)$ evaluated from soft x-ray profile is **more peaked by a factor of 2** inside the ITB than $n_e(r)$.
- $n_{Ar}/n_e \sim 1\%$ in the center and **0.5%** outside the ITB from Bremsstrahlung.

- $P_{rad}^{Ar} \sim 0.4 P_{rad}^{SOL+DIV}$.

WEDGE

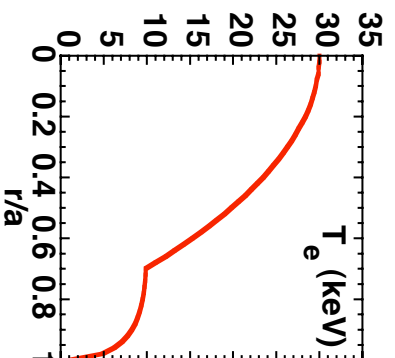
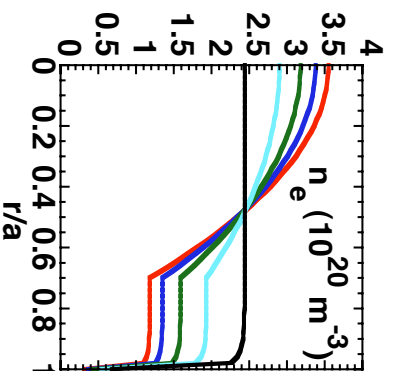
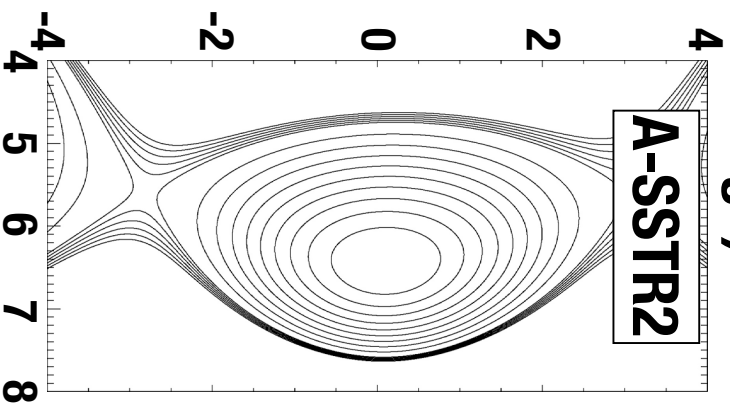


$n_{Ar}/n_e = 0.93\%$

Core radiation loss from Ar can be compensated with slightly enhanced confinement in a fusion reactor.

JT-60U

- Edge density can be reduced by density peaking.
- $HH_{y2}=1.4-1.5$ with more peaked $n_{Ar}(r)$ by a factor of 2 than $n_e(r)$.
- $Z_{eff}=4$ for 400MW radiation (0.5% Ar at edge).

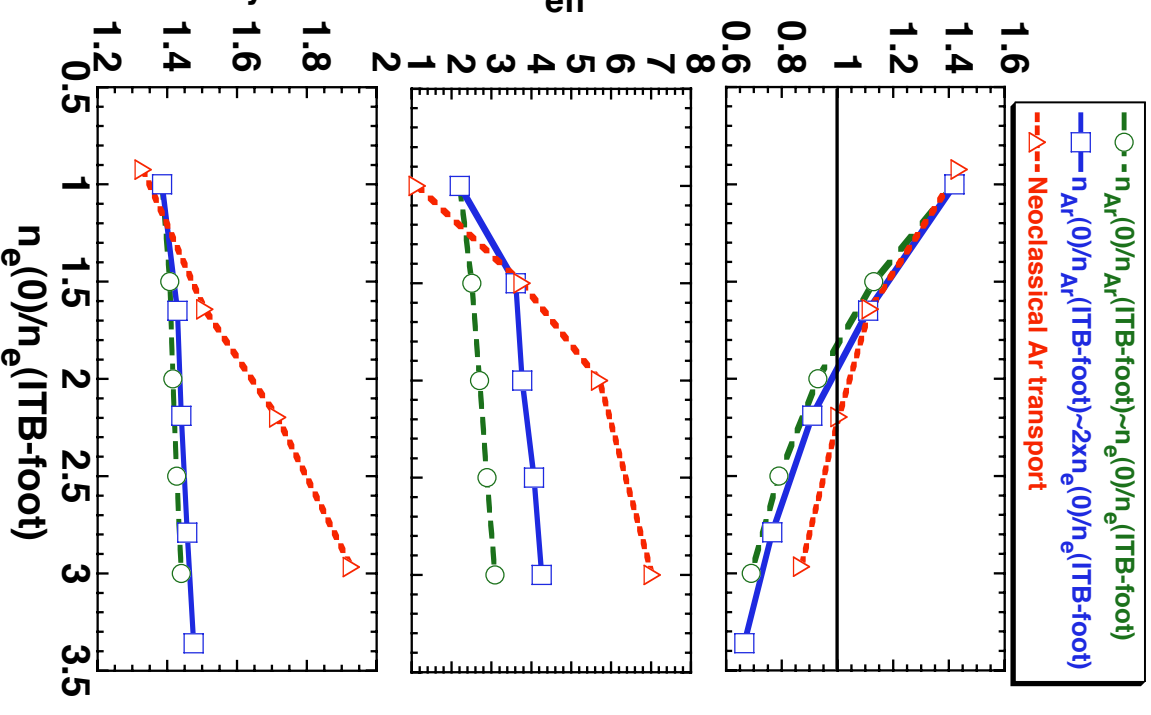


$I_p=12MA$, $B_T=11T$, $R_p=6.2m$,
 $a=1.5m$, Fusion output $\sim 4GW$,
 $P_{rad}^{main} \sim 400MW$,
 Aux. heating=60MW

n_e^{ped}/n_{GW}

Z_{eff}

HH_{y2}



Summary

JT-60U

- Operation regime of advanced tokamak plasmas has been extended.
- RS : $n_e/n_{GW}=1$, $HH_{y2}=1.2$, $P_{rad}^{main}/P_{abs} \sim 0.8$.
 $n_e/n_{GW}=1.1$, $HH_{y2}=1.1$, $f_{rad}=0.93$ with enhanced P_{rad}^{div} by Ne seeding
- High β_p H : $n_e/n_{GW}=0.92$, $HH_{y2}=0.96$, $f_{rad} \sim 1$ with HFS pellet and Ar seeding
- In both RS and high β_p H-mode plasmas, the high n_e/n_{GW} is achieved due to a peaked density profile inside the ITB.
- Ar accumulation by a factor of 2, as observed in the high β_p H-mode plasma, is acceptable in a fusion reactor for impurity seeding.
- Future work
 - Density ITB formation under the low central fueling.
 - Optimization of radiation ratio for main and Div.&SOL plasmas.